

### Labs test plan, phase 2 results analysis

Dec 9, 2020 Claude Chanson





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Labs test plan

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### General Status of Informal Working Group (IWG) and Test Group

- Last IWG meeting held in Arlington, Texas USA (October 2019)
  - Reviewed data on first round of testing from 7 labs
  - All labs received from PRBA same Li ion cell designs from same manufacturers, tested at 100% state of charge
  - See UN/SCETDG/56/INF.33 for minutes of Arlington meeting
- IWG meeting scheduled for September 2020 in Brussels cancelled due to COVID-19 pandemic
- Test Group meeting scheduled for May 2020 also cancelled, continued web-based meetings, developed second round of tests
  - Additional Li ion cells provided by PRBA to 8 labs, tested at different states of charge
  - Partial results provided today for review by IWG
- Next IWG planned for December 2020 after UN Sub-Committee meeting





#### Test plan phase 1

 Phase 1: Test of repeatability: 7 labs tested propagation in a row of 6 cells, 3 répétitions of test for pouch and cylindrical, at 100% SOC.





### Test plan phase 2

- test of effect of heating rate and SOC on propagation for 6 cells in a row (for test labs without gaz analysis, test series 2 and 5): received partial tests of 4 labs has of sept 1.
- test of effect of heating rate and SOC on propagation on gaz hazards, single cell test (for labs with gaz analysis, test series 4 and 6): received partial test of 2 labs has of Sept 1.

Experimental Procedure test series 2-5:

- Charge cells to SoC as in table below
- Heat cells according to Table 1.
- Each test is performed once

Table 1

	20% SoC	30% SoC	50% SoC	70% SoC	100% SoC
5 C/min					Priority #3
20 C/min	Priority #1	Priority #5	Priority #2	Priority #4	



### Test phase 2 results: table completed with all results received as of Dec 7<sup>th</sup> 2020

cyclindrical	2450 mAh																	
Pouch	4800 mAh									based on th	e reading of	the thermoco	uple opposite	side of the in	nitiation cell.			
										time of TR	Cell 2	Cell 3	Cell 4	Cell 5	Cell 6	Cell 1	Cell 2	Cell 3
	<ul> <li>cell type</li> </ul>	<ul> <li>heating device type</li> </ul>	Heating power -	heating ra 🔻	SOC -	max temp 👻	Temp 3rd 👻	compressi 🤻	Closed cha	seconds	delta sec 🔻	delta sec 🔻	delta sec 🔻	delta sec 🔻	delta sec 🔻	Max temp 👻	Max temp 👻	Max
L1-1	NMC/cylindrical	Omega heating pad (2,5 x 5	20	10	100	838			N	105	0 28	3 110	194	163	33	711	793	3
L1-2	NMC/cylindrical	Omega heating pad (2,5 x 5	20	11	. 100	815			N	110	2 9	9 67	42	106	187	722	815	5
L1-3	NMC/cylindrical	Omega heating pad (2,5 x 5	20	19	100	867			N	65	0 29	22	92	77	56	i	834	4
L1-4	NMC/Pouch	Omega heating pad (5 x 5 cr	40	5	100	850			N	220	8 4	1 5	5	4	5	534	1400	Ĵ
L1-5	NMC/Pouch	Omega heating pad (5 x 5 cr	n 40	9	100	825			N	121	2 4	1 2	. 1	91	2	794	825	5
L2-1	NMC/cylindrical	heating tape		10,7	100	984			N	60	0 2	2 13	133	1	50	984	879	e
L2-2	NMC/cylindrical	heating tape		10,9	100	909			N	60	0 0	) (	1	33	16	826	879	э
L2-3	NMC/Pouch	heating tape		9,6	100	841			N	90	0					784	780	J
L2-4	NMC/Pouch	heating tape		10,2	100	1012			N	90	0 1	L 1	. 6	6	2	928	988	3
L3-1	NMC/cylindrical	25 Watt cartirdge heater (4	heaters utilized)	20,9	100	853			Y	57	5 96	5 17	60	12	14	853	825	5
L3-2	NMC/cylindrical	25 Watt cartirdge heater (4	heaters utilized)	18	100	932			Y	43	3 94	1 8	25	17	23	761	. 932	2
L3-3	NMC/cylindrical	25 Watt cartirdge heater (4	heaters utilized)	20,9	100	848			Y	58	1 82	2 15	15	16	14	848	842	2
L3-4	NMC/Pouch	Capton Heaters, 2in. X 2in.,	10W/Sq.In. (2 heat	17,5	100	826			Y	57	7 43	3 6	i 4	. 9	8	785	805	5
L3-5	NMC/Pouch	Capton Heaters, 2in. X 2in.,	10W/Sq.In. (2 heat	20,5	100	826			Y	51	5 7	7 5	i 4	1	. 6	1034	819	э
L3-6	NMC/Pouch	Capton Heaters, 2in. X 2in.,	10W/Sq.In. (2 heat	15,8	100	826			Y	58	6 5	5 3	1	. 1	. 0	871	. 1164	4
L4-1	NMC/cylindrical	Kapton thermal pad (Omega	a) 10W/Inch2 (1Inc	10	100	1000			N	213	5 12	2 21	. 33	84	33	900	900	J
L4-2	NMC/cylindrical	Kapton thermal pad (Omega	a) 10W/Inch2 (1Inc	10	100	1000			N	212	1 13	3 20	34	82	35	620	900	J
L4-3	NMC/cylindrical	Kapton thermal pad (Omega	a) 10W/Inch2 (1Inc	10	100	1000			N	243	8 2	2 53	50	92	120	1000	1000	J
L4-4	NMC/Pouch	Kapton thermal pad (Omega	a)	10	100	2,5			N	240	0 10	7 0	5	5	4	750	850	J
L4-5	NMC/Pouch	Kapton thermal pad (Omega	a)	10	100	2,5			N	503	0 7	7 5	3	6	3	1000	900	J
L4-6	NMC/Pouch	Kapton thermal pad (Omega	a)	10	100	2,5			N	495	5 10	) 5	5	2	2	800	840	J
L5-1	NMC/cylindrical	Minco		18	100	850	35		Y	98	2 6	5 2	44	2	2	730,7	855,9	e
L5-2	NMC/cylindrical	Minco		18	100	769	35		Y	61	4					769,1	. 101,4	1
L5-3	NMC/Pouch	Minco (x3)		7	100	832	122		Y	159	3 5	5 6	6	12	13	643,1	. 772,7	1
L6-1	NMC/cylindrical	Heating pad (thin film)		7	100	1800			N	127	8 43	3 49	38	83	32	1294	1320	J
L6-2	NMC/cylindrical	Heating pad (thin film)		7	100	1800			N	113	0					1130	135	i
L6-3	NMC/Pouch	Heating pad (thin film)		10	100	780			N	163	9 8	3 6	6	8	9	680	780	J
L6-4	NMC/Pouch	Heating pad (thin film)		8	100	860			N	167	5 5	5 3	10	4	. 9	860	834	1
L7-1	NMC/cylindrical	Heating pad (30x30 mm, 20)	W)	20	100	802			N	25	8 74	1 24	35	24	50	802	736	5
L7-2	NMC/cylindrical	Heating pad (30x30 mm, 20)	W)	20	100	904			N	48	2 5	5 27	28	14	30	904	718	3
L7-3	NMC/cylindrical	Heating pad (30x30 mm, 20)	W)	20	100	810			N	37	8 11	L 34	53	18	28	764	717	1
L7-4	NMC/Pouch	Heating pad (70x60 mm, 55)	W)	15	100	935			N	77	0 5	5 3	3	2		935	924	4
L7-5	NMC/Pouch	Heating pad (70x60 mm, 55)	W)	15	100	1331			N	64	0 4	1 4	4	4		863	1331	1
L7-6	NMC/Pouch	Heating pad (70x60 mm, 55)	W)	15	100	1352			N	60	5 4	1 4	5	3		1352	912	2
L1-21	NMC/cylindrical	Omega heating pad (2,5 x 5	20	5	100	669	50	briks	Y	198	0 62	2 31	. 81	22	7	669	757	1
L1-22	NMC/cylindrical	Omega heating pad (2,5 x 5	20	14	- 70	738	33	briks	Y	771,42857	1 120	120	0	170	122	737,91	617,32	2
L1-23	NMC/cylindrical	Omega heating pad (2,5 x 5	20	20	50	578	29	briks	Y	50	4 353	3 265	267	264	268	556,71	561,42	2
L1-24	NMC/cylindrical	Omega heating pad (2,5 x 5	20	20	20	200		briks	Y		0 0	) (	0	0	0	361	. 213	3





#### Phase 1 results analysis: Max temperature

Typical max temperature for both type of cells is about 900°C stdandard deviation around 100°C.

Cylindrical

Pouch





the temperature increase represents an amount of energy of 1.2 MJ/kg (including the contained electrical energy of around 0.6 MJ/kg) . This value is well correlated with literature data.

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#### Phase 1 results analysis: Propagation time

- Very different typical time for cyl and pouch cells, due to larger surface of contact

Cylindrical



Pouch

Dispertion observed due to lack of reproducible compression, cells core ejections for cyclindircal cells





# Phase 1 results analysis: TR onset temperature

- Typical temperature of onset around 180°C for pouch, more dispersion with cyclindrical

Pouch

Cylindrical



Dispertions observed due to various methods for measure, and dynamics of the TR.



### Phase 1 results analysis: TR onset temperature correlation with heating rate

- At 100% SOC, No clear correlation

Cylindrical

Pouch





# Representativeness of the TR obtained with the heater: propagation rate

- At 100% SOC, Pouch cells, no difference between cell2 and 6 in a row. for the propafation time, despite pre-heating observed.





"L1-2": means test of laboratory 1, test number 2. The individual test result for each cell is represented by a single bar. Cell 1 is the initiation cell, cell 2 the next cell in the row, etc...



### Representativeness of the TR obtained with the heater: max temperature

- At 100% SOC, non difference observed between initiation cell and others cells

Pouch

Cylindrical





# Phase 1 results analysis: repeatability and reproducibility

- Repetability (per lab): stability of averages and standard deviation and reproducibility (between labs): stability of averages and standard deviation:.
- The Repeatability and Reproducibility are combined to assess the total potential variations of a measured result, in the R&R approach





### **R&R** for max temperature

main source of variation for the measure of the maximum temperature is the **reproductibility**, for both type of cells: the repeatability (variation within each laboratory) is in the range of 50°C (about 6% of the average), but the R&R, including the reproducibility (variations between labs average) is more than 100°C. It supports the need to better harmonize the conditions of test between the labs to achieve a better reproducibility (effect of lid!).

Pouch

Cylindrical



### **R&R for propagation rate**

The more important variation source for the propagation time is the lack of **repeatability,** particularly for the cylindrical cells (67% of the average time). This indicates that the test conditions should be specified more precisely, such has the compression between cells in the case of cylindrical cells.

Pouch

Cylindrical



Note: L1-2 means « laboratory 1 test 2 »



### Phase 2 results analysis: effect of SOC on max Temp

- Stability of the max temperature during self propagation at various SOC: the initiation method seems of little impact on the reaction, except in absence of propagation (20% SOC)







### Phase 2 results analysis: effect of SOC on max Temp, reproducibility

- But repetability within a lab is much better than reproducibility interlabs, particumarly at intermediate SOC 30-50%

Results of 1 lab

Results of 3 labs at 50% SOC







### Phase 2 results analysis; effect of SOC on max temp, all results

Dispersion increases at the point of transition for propagation (30-50% SOC). In case of propagation, the max temp is not much reduced between 100% and 50% SOC.

Pouch

Cylindrical





The cell voltage indicates the SOC (20% to 100% corresponds to 3,6V to 4,15V)

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# Phase 2 results analysis; effect of SOC on propagation time

- Contrary to max temperature, propagation time is changing when measured in a same laboratory.





First 100% soc is average of phase 1. The three at 50% SOC are 3 different labs

# Phase 2 results analysis; effect of SOC on propagation time and onset temperature, all results

Due to the lack of repeatability, the effect is less clear for all labs







### Phase 2 results analysis: gaz analysis under Nitrogen atmosphere.

At higher state of charge, the volume of gaz generated is higher, and the gaz composition is less oxidized (hydrogen content is higher and ratio CO/CO2 is higher). As a result, it can be concluded that at higher SOC, the gaz hazard due to flammability or explosion properties will increase







### Phase 2 results analysis: gaz analysis under air atmosphere, effect of SOC.

the same results were observed as in propagation test: no significant effect of the heating rate on the TR maximum and onset temperatures, but a significant effect of the high SOC, reducing the onset temperature and increasing the TR maximum temperature







### Phase 2 results analysis: gaz analysis under air atmosphere, effect of SOC.

the same results were observed as in propagation test: no significant effect of the heating rate on the TR maximum and onset temperatures, but a significant effect of the high SOC, reducing the onset temperature and increasing the TR maximum temperature







### Phase 2 results analysis: gaz analysis under air atmosphere, of heating rate

The quantity of gaz emitted is higher at higher SOC. Nevertheless, the emitted gaz volume is sensitive to the heating rate only at higher SOC, with a factor almost 2 between 5 and 20°C/min







#### **Other relevant data**

See

- CATL presentation about large cells testing (Oct 2019)
- LG data about vrious cells testing (Dec 2020)
- FAA presentation about gaz production (ref?)



### Preliminary conclusions, for discussion

#### About the lithium batteries hazards characterization

- The test have been affected by the lack of reproducibility due to variations in the tests methods applied by various labs, but tests demonstrate some level of repeatability of the Thermal runaway hazards: max temperature, onset temperature, gaz volumes, gaz composition.
- Some key parameters influencing the hazards per cell, and their propagation, are tested: cell format, cell SOC, heating rate.
- The analysis of specific toxicity (i.e. HF and HCNcontent), has shown lack of repeatability (within lab) and reproducibility between labs due to various analytical methods. Only a typical range of composition can be assessed.



### Preliminary conclusions, for discussion

#### About the test method:

-the heater method provides a reproducible way to initiate a thermal runaway. Limit of conditions would need to be made more specific to increase repeatability: heating rates, heater types, compression between cells.

-the TR obtained by the heater is close to the one obtained by selfpropagation, although the propagation time is very different, demonstrating some robustness of the method.

-A larger dispersion in results is observed when the TR energy is closer to the boundary of non-propagation. The results also indicates that the heating method induces a TR for cells having not enough reaction energy to propagate. In this case, the result obtained is more severe than the expected result of an internal short circuit



### Preliminary conclusions, for discussion

#### About the reproducib:

There are much more difference between labs than within a single lab.

The test decription will have to be more specific and precise:

#### Identified effect of :

- absence of lid on the test chamber
- various efforts for cells compression during test
- (Partially) heating rate range
- Method for identification (max temperature, onset temperature,..)
- Others to be discussed...



#### **Next steps**

-Complete the tests table and analysis (anonymized labs names): done

- -Circulate to all labs for review
- -pending issues for the December Meeting
  - hazards characterization
  - method description
  - labs comparison
- -Others?

